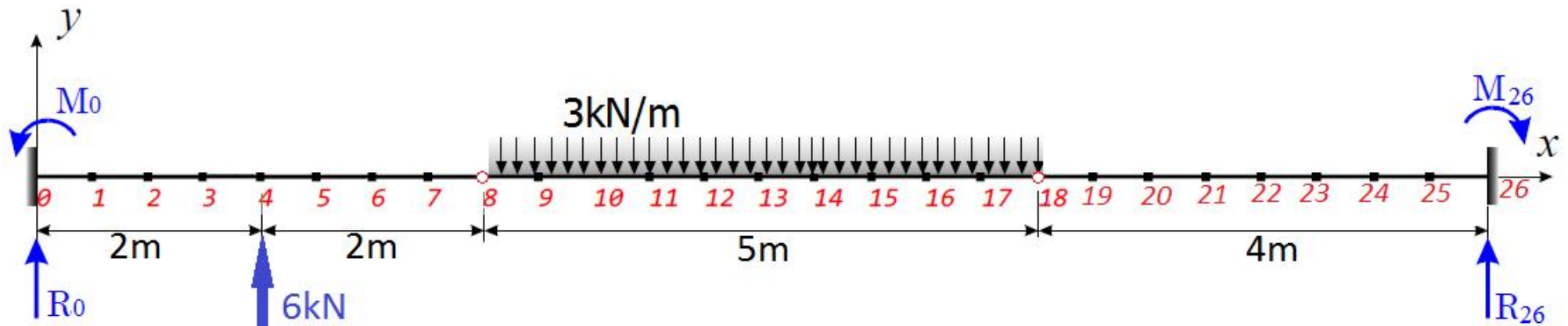


Obliczenie ugięcia belki metodą różnic skończonych (MRS)

ORIGIN := 0



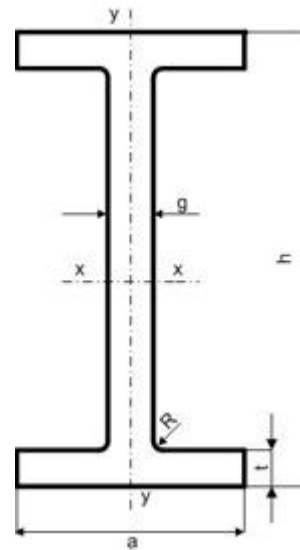
Przekrój poprzeczny belki - IPE160

$$a := 82\text{mm} \quad g := 5\text{mm} \quad t := 7.4\text{mm} \quad h := 160\text{mm}$$

$$a1 := a - g \quad h1 := h - 2 \cdot t$$

$$A := a \cdot h - a1 \cdot h1 \quad J := \frac{a \cdot h^3 - a1 \cdot h1^3}{12}$$

$$E := 210\text{GPa} \quad \gamma := 78 \frac{\text{kN}}{\text{m}^3}$$



$$q := 3 \frac{\text{kN}}{\text{m}} \quad p := A \cdot \gamma = 0.151 \cdot \frac{\text{kN}}{\text{m}} \quad P := 6 \text{ kN} \quad L := 13 \text{ m} \quad L1 := 2 \text{ m} \quad L2 := 5 \text{ m} \quad L3 := 4 \text{ m}$$

$$T8 := \frac{L2 \cdot (q + p)}{2} \quad T18 := T8 \quad - \text{siły poprzeczne w przegubach}$$

$$R0 := T8 + p \cdot L3 - P \quad R26 := T18 + L3 \cdot p \quad - \text{reakcje podpór}$$

$$M0 := T8 \cdot L3 + p \cdot \frac{L3^2}{2} - P \cdot L1 \quad M26 := T18 \cdot L3 + p \cdot \frac{L3^2}{2} \quad - \text{momenty podporowe}$$

$$\Delta := 0.5 \text{ m} \quad \alpha := \frac{\Delta^2}{E \cdot J} \quad n := \frac{L}{\Delta} = 26 \quad i := 0 .. n \quad X_i := i \cdot \Delta \quad - \text{współrzędne punktów węzłowych}$$

$$M1(x) := -M0 + R0 \cdot x - p \cdot \frac{x^2}{2} \quad i := 0 .. 4 \quad M_i := M1(X_i) \quad - \text{momenty zginające w przedziale nr 1}$$

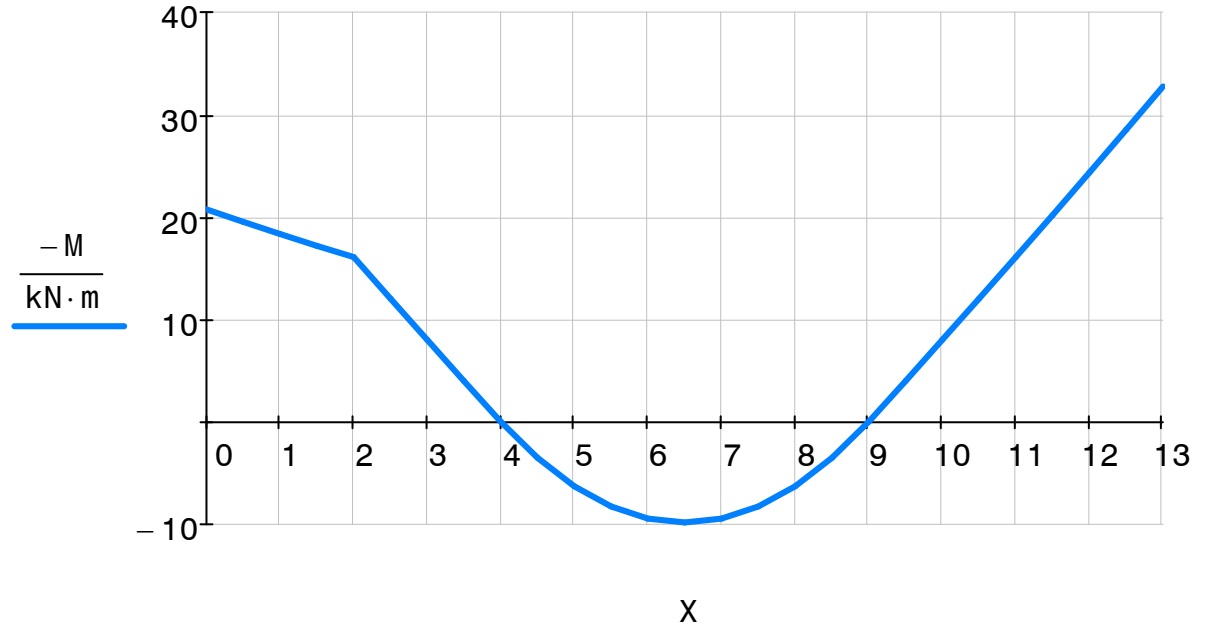
$$M2(x) := M1(x) + P \cdot (x - L1) \quad i := 5 .. 8 \quad M_i := M2(X_i) \quad - \text{momenty zginające w przedziale nr 2}$$

$$M3(x) := M2(x) - q \cdot \frac{(x - L3)^2}{2} \quad i := 9 .. 18 \quad M_i := M3(X_i) \quad - \text{momenty zginające w przedziale nr 3}$$

$$M4(x) := M3(x) + q \cdot \frac{(x - L3 - L2)^2}{2} \quad i := 19 .. n \quad M_i := M4(X_i) \quad - \text{momenty zginające w przedziale nr 4}$$

Wykres momentów zginajających

| | 0 | | 0 |
|-----|--------------------------|-----|------|
| M = | -20.723 | X = | 0 |
| | -19.5 | | 0.5 |
| | -18.315 | | 1 |
| | -17.168 | | 1.5 |
| | -16.059 | | 2 |
| | -11.988 | | 2.5 |
| | -7.954 | | 3 |
| | -3.958 | | 3.5 |
| | -1.819·10 ⁻¹⁵ | | 4 |
| | 3.545 | | 4.5 |
| | 6.303 | | 5 |
| | 8.272 | | 5.5 |
| | 9.454 | | 6 |
| | 9.848 | | 6.5 |
| | 9.454 | | 7 |
| | 8.272 | | 7.5 |
| | 6.303 | | 8 |
| | 3.545 | | 8.5 |
| | 0 | | 9 |
| | -3.958 | | 9.5 |
| | -7.954 | | 10 |
| | -11.988 | | 10.5 |
| | -16.059 | | 11 |
| | -20.168 | | 11.5 |
| | -24.315 | | 12 |
| | -28.5 | | 12.5 |
| | -32.723 | | 13 |



Macierz układu równań MRS:

$$i := 0.. n \quad A_{i, i} := -2 \quad i := 1.. n \quad A_{i, i-1} := 1 \quad i := 0.. n-1 \quad A_{i, i+1} := 1$$

A =

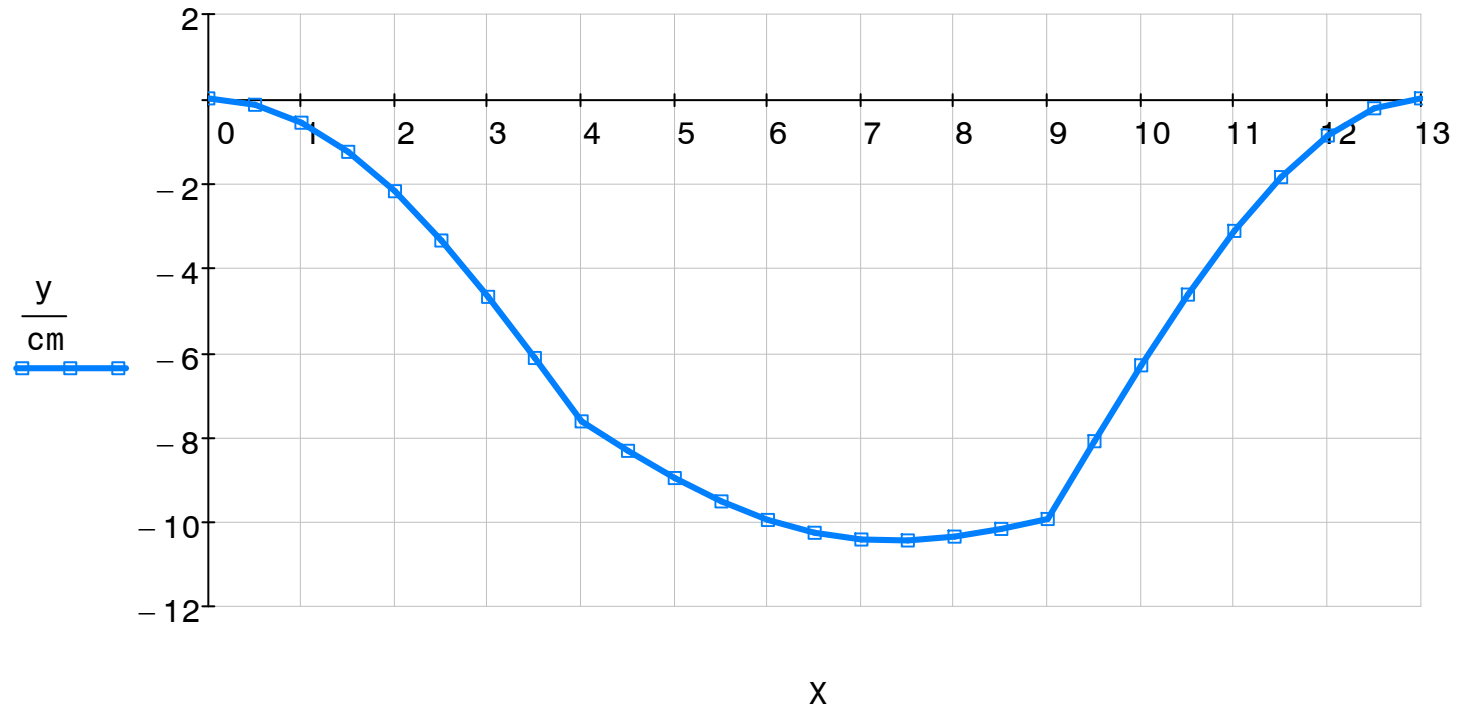
| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|---|
| 0 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 1 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 | 0 |
| 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 | 0 |
| 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 | 0 |
| 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 | 0 |
| 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | 1 |

$$y := \text{lsolve}(A, \alpha \cdot M)$$

Wykres ugięć belki

| | |
|----|---------|
| | 0 |
| 0 | 0.000 |
| 1 | -0.148 |
| 2 | -0.574 |
| 3 | -1.261 |
| 4 | -2.193 |
| 5 | -3.354 |
| 6 | -4.686 |
| 7 | -6.132 |
| 8 | -7.634 |
| 9 | -8.328 |
| 10 | -8.972 |
| 11 | -9.527 |
| 12 | -9.963 |
| 13 | -10.264 |
| 14 | -10.425 |
| 15 | -10.451 |
| 16 | -10.359 |
| 17 | -10.177 |
| 18 | -9.944 |
| 19 | -8.100 |
| 20 | -6.312 |
| 21 | -4.638 |
| 22 | -3.134 |
| 23 | -1.860 |
| 24 | -0.873 |
| 25 | -0.233 |
| 26 | 0.000 |

$y =$ $\cdot \text{cm}$



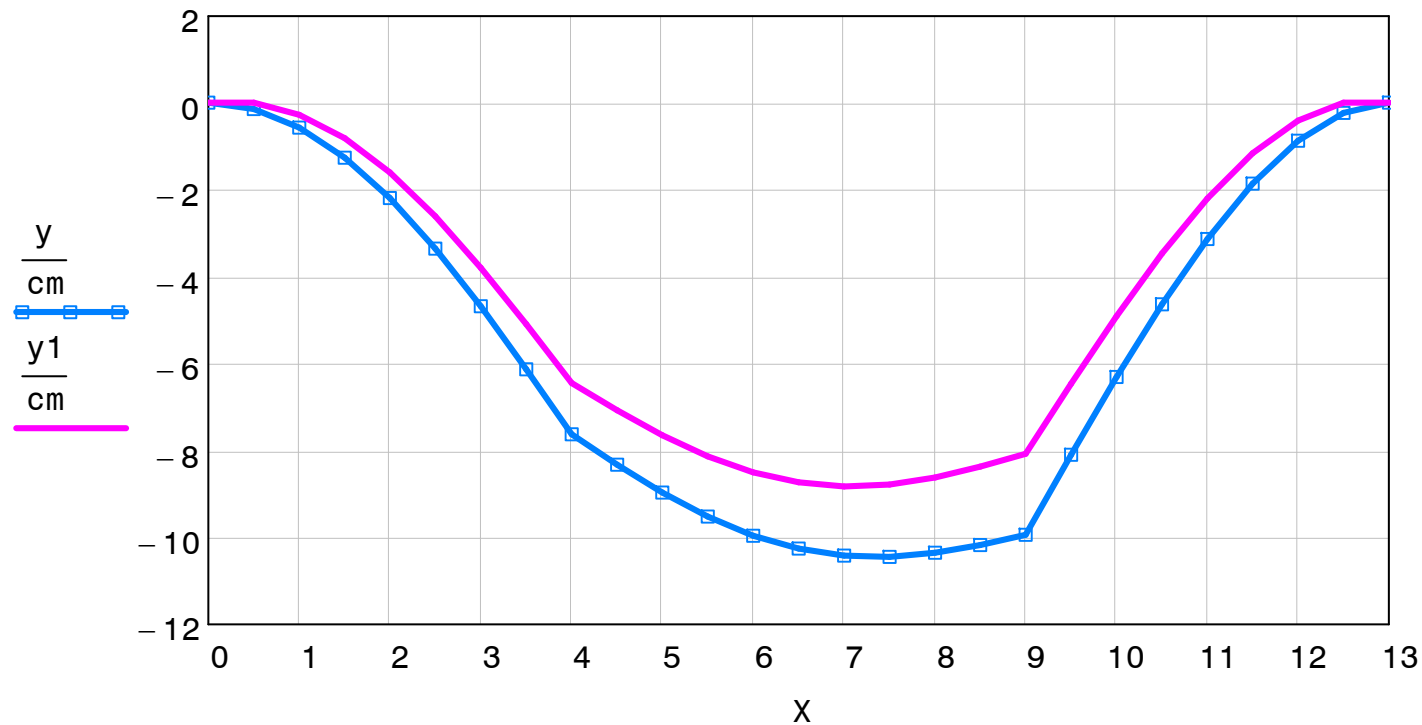
Ma := M Ma₀ := 0 Ma_n := 0

y1 := lsolve(A, α · Ma)

*Wykres ugięć belki - porównanie zastosowania 2 sposobów
uwzględniania warunku brzegowego: φ=0,
y - różnica centralna, y1 - różnica "w przód"*

| | |
|----|--------|
| | 0 |
| 0 | 0.000 |
| 1 | 0.000 |
| 2 | -0.278 |
| 3 | -0.818 |
| 4 | -1.602 |
| 5 | -2.615 |
| 6 | -3.799 |
| 7 | -5.097 |
| 8 | -6.451 |
| 9 | -7.078 |
| 10 | -7.653 |
| 11 | -8.139 |
| 12 | -8.507 |
| 13 | -8.739 |
| 14 | -8.832 |
| 15 | -8.789 |
| 16 | -8.629 |
| 17 | -8.378 |
| 18 | -8.077 |
| 19 | -6.467 |
| 20 | -4.912 |
| 21 | -3.471 |
| 22 | -2.201 |
| 23 | -1.160 |
| 24 | -0.407 |
| 25 | 0.000 |
| 26 | 0.000 |

y1 = · cm



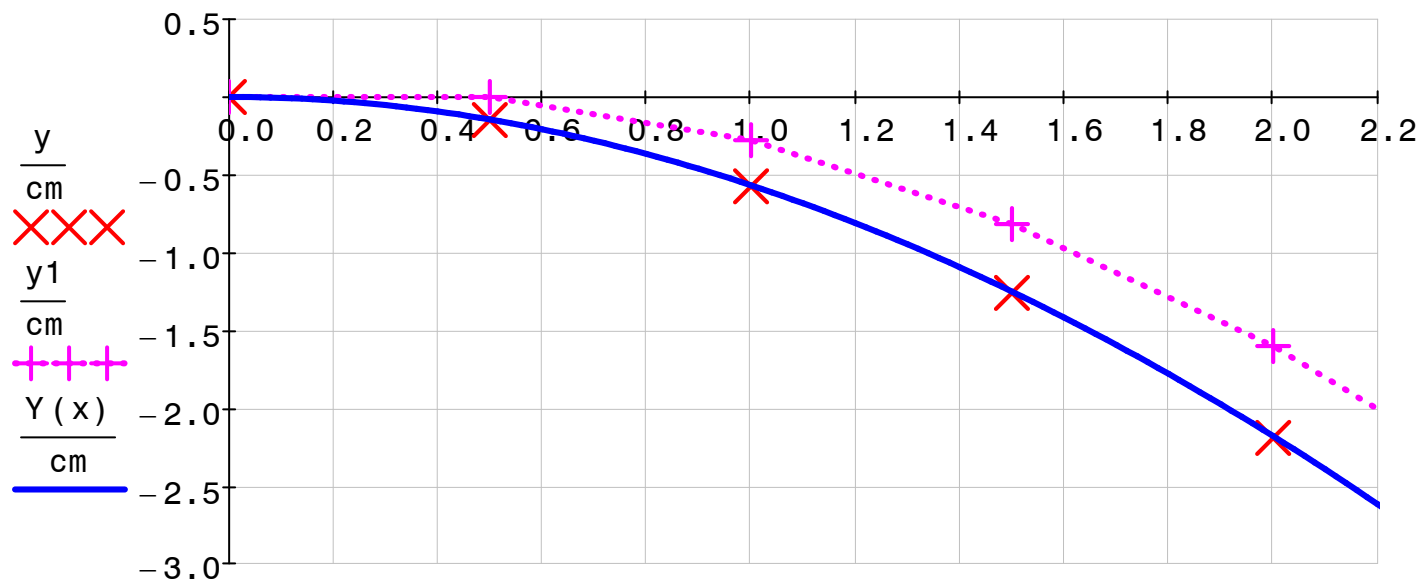
$$\Phi(x) := \frac{1}{E \cdot J} \cdot \int_0^x M1(z) dz$$

$$Y(x) := \int_0^x \Phi(z) dz$$

$$Y4 := Y(L1) = -2.182 \text{ cm}$$

Wykres ugięć belki - porównanie wyników uzyskanych numerycznie z rozwiązaniem analitycznym $Y(x)$ w przedziale nr 1.

Widoczne są duże błędy rozwiązania numerycznego $y1$, uzyskanego przy zastosowaniu różnicy "w przód"



Błędy rozwiązań numerycznych

$$\varepsilon := \frac{y4}{Y4} - 1 = 0.525\%$$

$$\varepsilon1 := \frac{y14}{Y4} - 1 = -26.574\%$$

$$\frac{X}{m}, \frac{X}{m}, \frac{x}{m}$$